

Job No: 1010577.2000

15 June 2021

New Zealand Steel Ltd Private Bag 92121 Auckland

Attention: Claire Jewell

Dear Claire

### NZ Steel - Glenbrook Steel Mill Structural Inspection of Southside and Northside Outfalls

### 1 Introduction

NZ Steel Ltd engaged Tonkin & Taylor Ltd (T+T) to undertake a structural inspection of two outfall structures at the NZ Steel Glenbrook site (hereafter referred to as the Southside and Northside Outfalls). The inspection was undertaken to support NZ Steel's application to seek coastal occupation permits for the Southside and Northside Outfalls.

This report summarises the findings of our structural inspection, and includes commentary on the expected structural integrity of the outfalls over the term of the consent (up to 35 years), including the effects of predicted sea level rise.

The inspection was undertaken by a T+T Chartered Structural Engineer on 20 January 2021, at approximately low tide.

Selected photographs from the inspection, together with the available drawings of the outfalls, are attached to this report as Appendix B and Appendix C.

### 2 Level Survey Results

To confirm the extent that the outfalls will be within the Coastal Marine Area (CMA) over the 35 year term of the consent, a level survey was undertaken by LEH Surveyors in January 2021. Survey results are included in Appendix A, together with current and predicted future Mean High Water Springs (MHWS) levels provided by T+T.

The level survey results indicate the following:

#### Southside Outfall

- Current MHWS is 2.26 m AVD (Auckland Vertical Datum 1946).
- Predicted MHWS in 2055 is 2.49 m AVD.
- Top of outfall base slab (at its lowest tier) is 2.23 m AVD.

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The bottom of this slab is estimated at 2.13 m AVD, based on a slab thickness of 200 mm estimated from review of NZ Steel drawing 510/508/002/000/011 rev 0 (see Appendix C).

Therefore, the bottom of the lowest tier of the base slab (downstream of the weir) is currently 230 mm below MHWS, and therefore the Southside Outfall is currently within the CMA.

By 2055, the bottom of the lowest tier of the base slab will be 460 mm below the predicted MHWS.

#### Northside Outfall

- Current MHWS is 2.26 m AVD (Auckland Vertical Datum 1946).
- Predicted MHWS in 2055 is 2.49 m AVD.
- Top of outfall slab level is 2.34 m AVD.
- The bottom of the outfall slab level is estimated at 2.19 m AVD, based on a slab thickness of 150 mm as indicated on the T+T drawings of the outfall (see Appendix C).

Therefore, while the top of the base slab is currently 80 mm above MHWS, the bottom of the slab is currently 70 mm below MHWS. Therefore, the Northside Outfall is currently within the CMA.

By 2055, the bottom of the base slab will be 300 mm below the predicted MHWS.

### 3 Observations

#### 3.1 Southside Outfall

A drawing provided by NZ Steel (NZ Steel drawing ref 510/508/002/000/011 rev 0, attached in Appendix C) is dated June 1983, indicating that the outfall is approximately 37 years old. Observations on site indicate that the structure has not been substantively modified since the original design.

The outfall is constructed from a combination of reinforced concrete (headwall, weirs, base slab and adjacent side walls) and reinforced concrete masonry blocks (side walls on the downstream portion of the structure). Access across and around the outfall is provided by a timber pedestrian bridge and stairs. The area downstream of the structure is protected by a layer of riprap (noted as class II riprap on the drawing).

The reinforced concrete and concrete masonry elements were in good condition, with only minor historic shrinkage cracking and efflorescence (indicating localised dampness) visible on the exposed faces. Some evidence of a concrete repair was visible on the downstream face of the concrete wall forming the V-notch weir. Some minor damage was noted at the top of the northern side masonry wall.

The timber access structures were also in good condition, although some areas of corrosion were noted on steel barriers.

No evidence of scour or erosion was observed in the riprap area immediately downstream of the structure.

### 3.2 Northside Outfall

Drawings provided by NZ Steel (T+T drawing set titled "Woolf Fisher Works Settling Ponds Phase 1", ref 5384, attached in Appendix C) are dated 1983, indicating that the outfall is approximately 37 years old. A further drawing supplied by NZ Steel, drawing number 061/530/009/000/005 (see Appendix C), indicates that a new steel weir, pipework and a pump station were added to the outfall in 1988.

Observations on site indicate that the structure has not been substantively modified since the original design, other than the 1988 additions noted above.

The drawings indicate that the original design consisted of a reinforced concrete energy dissipator structure, upstream of a dispersal structure consisting of a reinforced concrete slab and reinforced concrete masonry side walls. Observations on site indicate that the dispersal structure side walls were subsequently constructed in reinforced concrete rather than concrete masonry.

A V-notch weir, spanning between the side walls and base slab, is constructed from steel plate, with diagonal steel struts providing additional lateral support. Various timber and steel platform / stair structures provide access over and around the outfall.

The reinforced concrete elements were in good condition, with only minor historic shrinkage cracking and discolouration (indicating localised dampness) visible on the exposed faces. The visible parts of the steel V-notch weir were in good condition. The steel platform above the outlet channel was showing signs of minor corrosion to some structural members.

The timber access structures were in good condition.

No obvious signs of erosion were noted immediately downstream of the outfall structure.

### 4 Commentary on Structural Integrity

#### 4.1 Southside Outfall

The concrete outfall structure was in good condition, with only minor evidence of concrete repair visible. Over the next 35 years, the condition of the structure can be expected to deteriorate somewhat, and some further concrete repairs could be required, based on our experience of coastal structures of comparable age. However, this deterioration is not expected to affect the structural integrity of the outfall, provided the repairs are undertaken in a timely fashion. The anticipated repairs would typically involve removing loose / cracked concrete, protecting / replacing corroded reinforcing as required, and reinstating using an approved repair mortar.

Sea level rise is predicted to result in more of the slab and side walls downstream of the weir being within the tidal range over the term of the consent (refer Section 2). The affected area may need a greater level of repairs due to the more aggressive tidal environment. However, the structural integrity of the outfall is not anticipated to be affected, provided the structure is maintained and repaired as required.

The timber / steel access structures are likely to need maintenance, and potentially full replacement, within the next 35 years, however this will not affect the structural integrity of the outfall.

The riprap is likely to need regular inspection and potential maintenance over the next 35 years, to ensure that undermining of the outfall structure does not occur due to scour.

### 4.2 Northside Outfall

The concrete outfall structure was in good condition. Over the next 35 years, the condition of the structure can be expected to deteriorate somewhat, and some further concrete repairs could be anticipated to be required, based on our experience of coastal structures of comparable age. However, this deterioration is not expected to affect the structural integrity of the outfall, provided the repairs are undertaken in a timely fashion. The expected repairs would typically involve removing loose / cracked concrete, protecting / replacing corroded reinforcing as required, and reinstating using an approved repair mortar.

Sea level rise is predicted to result in more of the slab and side walls downstream of the steel V-notch weir being within the tidal range over the term of the consent (refer Section 2). The affected area may need a greater level of repairs due to the more aggressive tidal environment. However, the structural integrity of the outfall is not anticipated to be affected, provided the structure is maintained and repaired as required.

The timber / steel access structures and the steel V-notch weir are likely to need maintenance, and potentially full replacement, within the next 35 years. However this will not affect the structural integrity of the outfall.

The channel immediately downstream of the outfall structure is likely to need regular inspection and potential maintenance over the next 35 years, to ensure that undermining of the outfall structure does not occur due to scour.

### 5 Applicability

This report has been prepared for the exclusive use of our client New Zealand Steel Ltd, with respect to the particular brief given to us and in accordance with the scope of work set out in our letter of engagement dated 17 June 2019 and associated variations. It may not be relied upon in other contexts or for any other purpose, or by any person other than our client, without our prior written agreement.

We understand and agree that our client will submit this report as part of an application for resource consent and that Auckland Council as the consenting authority will use this report for the purpose of assessing that application.

Tonkin & Taylor Ltd

**Environmental and Engineering Consultants** 

Report prepared by: Authorised for Tonkin & Taylor Ltd by:

Dale Vince

Structural Engineer

Jenny Simpson

M. Sus

Project Director

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Appendices:

Appendix A: Level Survey Results

Appendix B: Photographs Appendix C: Drawings

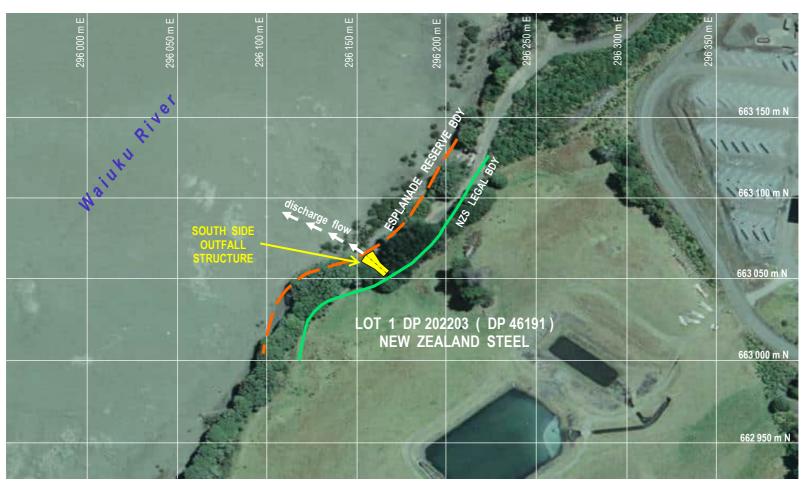
## Appendix A: Level Survey Results

## NZS - SOUTH SIDE OUTFALL STRUCTURE MHWS SURVEY SITE LOCALITY PLAN

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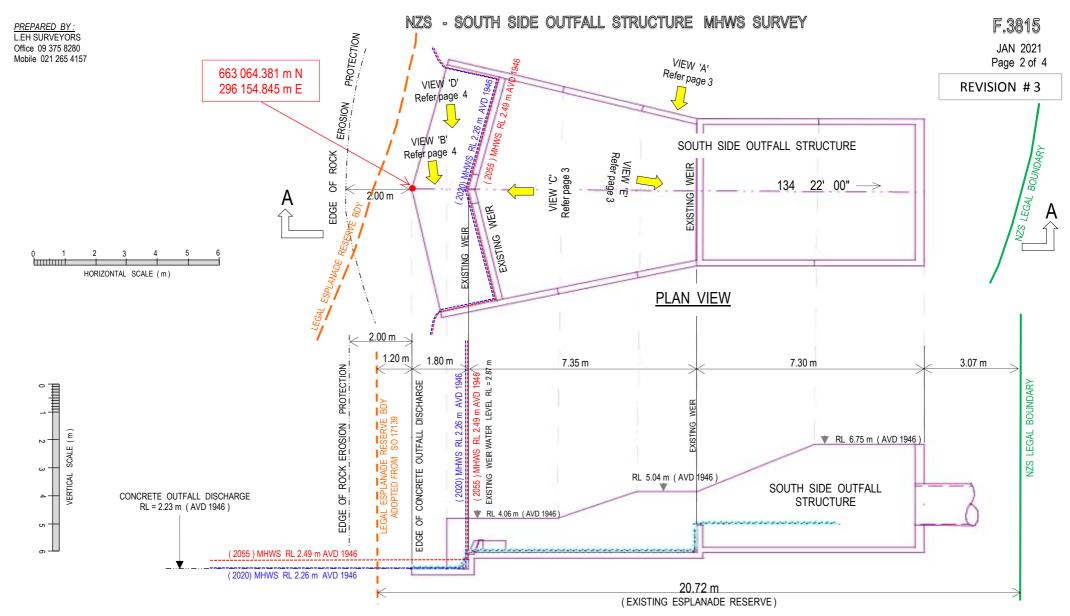
**REVISION #3** 



AERIAL PHOTO - PLAN VIEW

### NOTES:

- 1.- Co.ordinates are in terms with NZ Mount Eden Circuit Geodetic Datum 1949.
- 2.- Levels are in terms with 'Auckland Vertical Datum 1946.
- 3.- NZS Legal Boundary is in terms with DP 46191.
- 4.- Legal Esplanade Reserve Boundary is in terms with adoptions from SO 17139.



#### Future projected MHWS levels ( supplied by Tonkin & Taylor ) MHWS ( m AVD - 46 ) **PERIOD** Year Present 2020 2.26 m 2045 2.41 m 25 Years 2055 35 Years 2.49 m 100 Years 2120 3.23 m

## LONGITUDINAL SECTION THROUGH SOUTH SIDE OUTFALL STRUCTURE <u>ELEVATION 'A - A'</u>

#### NOTES:

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VIEW 'A'

VIEW 'C'



VIEW 'E'

### NZS - SOUTH SIDE OUTFALL STRUCTURE MHWS SURVEY

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REVISION #3



VIEW 'B'



VIEW 'D'

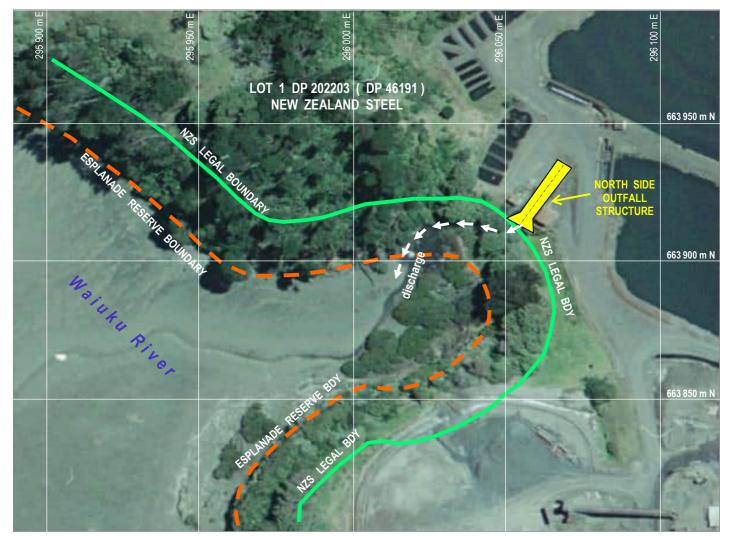
PREPARED BY: L.EH SURVEYORS Office 09 375 8280 Mobile 021 265 4157

## NZS - NORTH SIDE OUTFALL STRUCTURE MHWS SURVEY SITE LOCALITY PLAN

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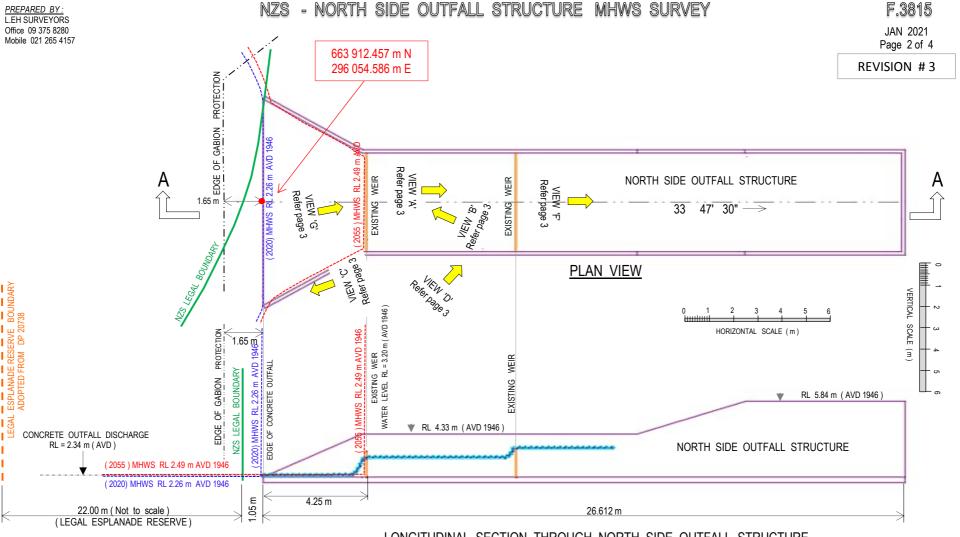
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AERIAL PHOTO - PLAN VIEW

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## LONGITUDINAL SECTION THROUGH NORTH SIDE OUTFALL STRUCTURE <u>ELEVATION 'A - A'</u>

Future projected MHWS levels ( supplied by Tonkin & Taylor )			
	<u>PERIOD</u>	<u>Year</u>	MHWS ( m AVD - 46 )
	Present	2020	2.26 m
	25 Years	2045	2.41 m
	35 Years	2055	2.49 m
	100 Years	2120	3.23 m

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- DENOTES REFERENCE DITIGAL PHOTO DIRECTION ( REFER PAGES 3 & 4)

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## NEW ZEALAND STEEL - NORTH SIDE OUTFALL STRUCTURE MHWS SURVEY REFERENCE DIGITAL PHOTOS

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REVISION #3





VIEW 'A'

VIEW 'G'





VIEW 'F'

VIEW 'C'

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# NEW ZEALAND STEEL - NORTH SIDE OUTFALL STRUCTURE MHWS SURVEY REFERENCE DIGITAL PHOTOS

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**REVISION #3** 



VIEW 'D'



VIEW 'B'

## Appendix B Photographs



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N3.JPG



N4.JPG



N5.JPG



N6.JPG



N7.JPG



N8.JPG



N9.JPG



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N23.JPC



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S2.JPG



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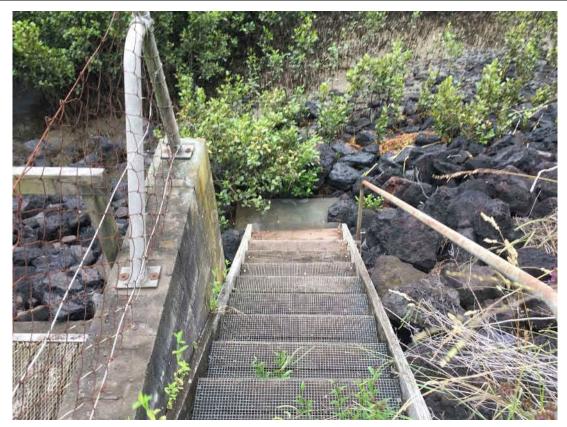
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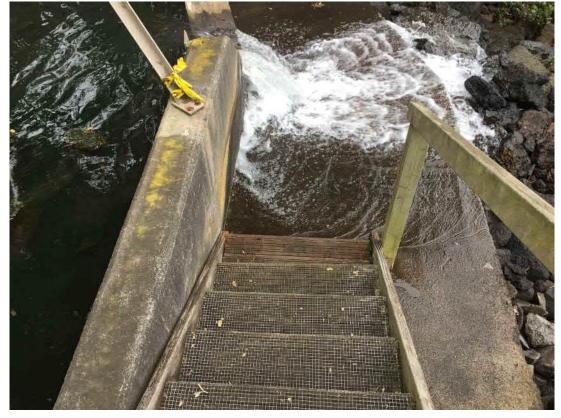
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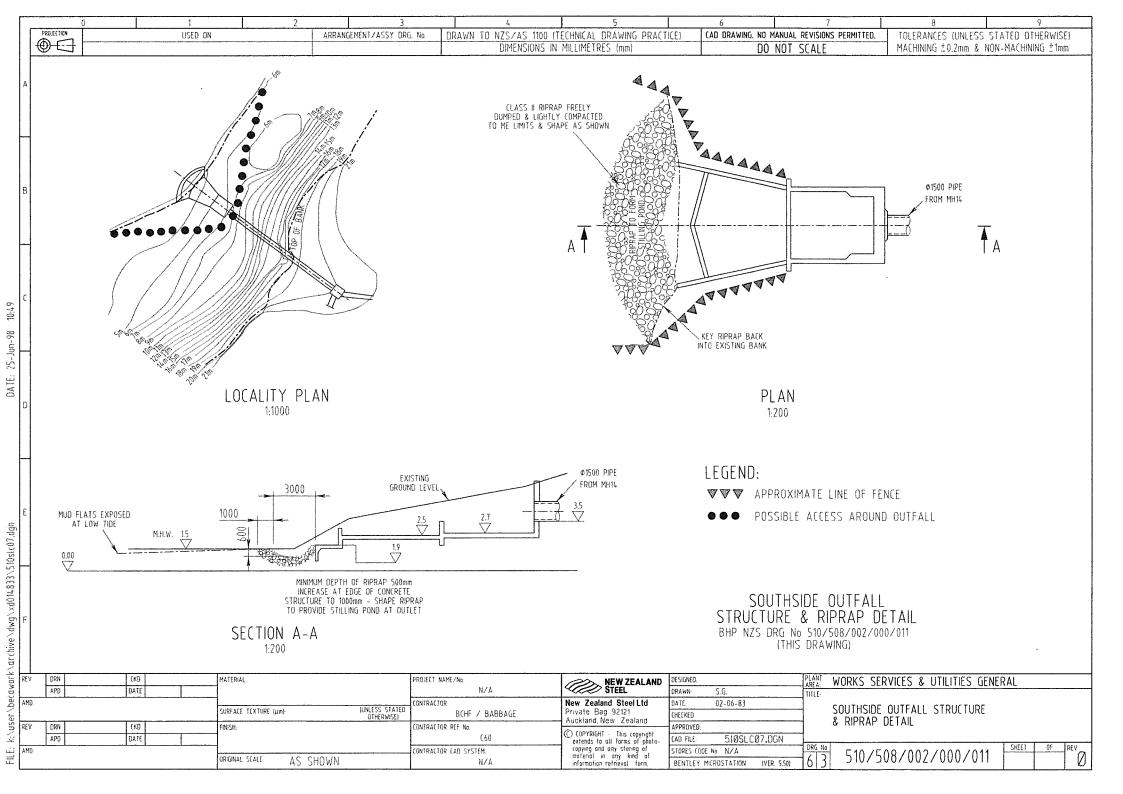


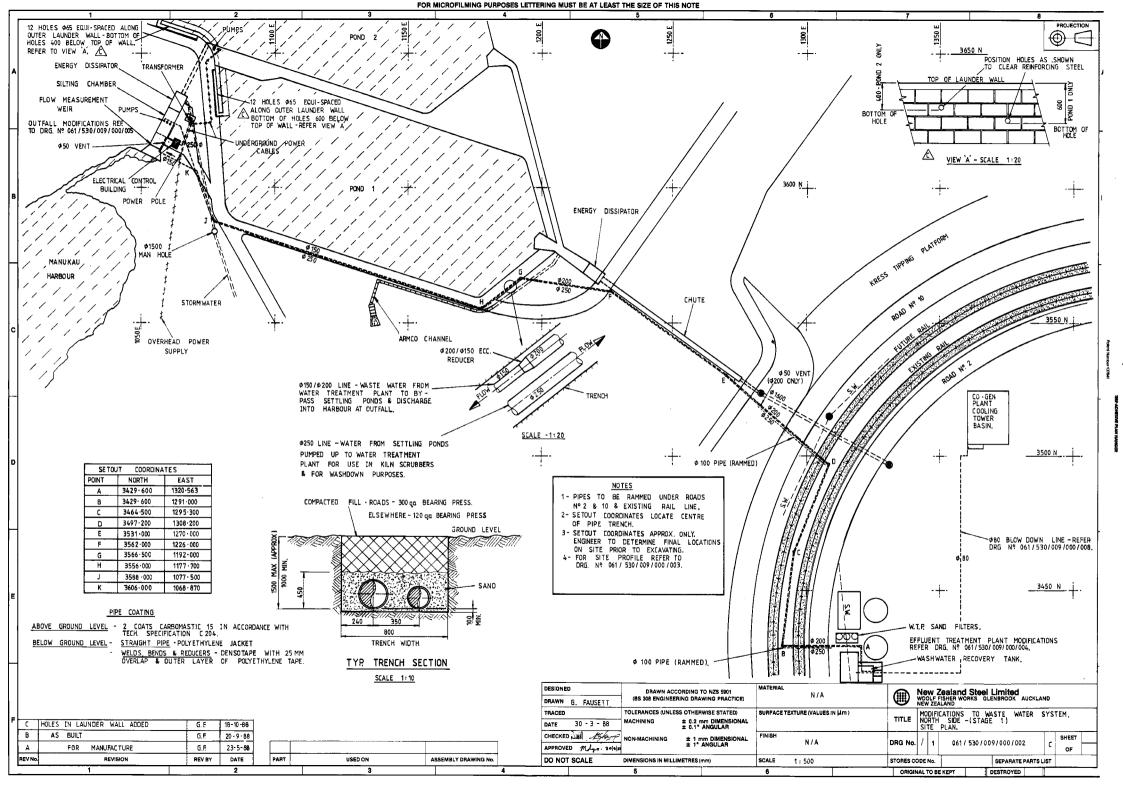
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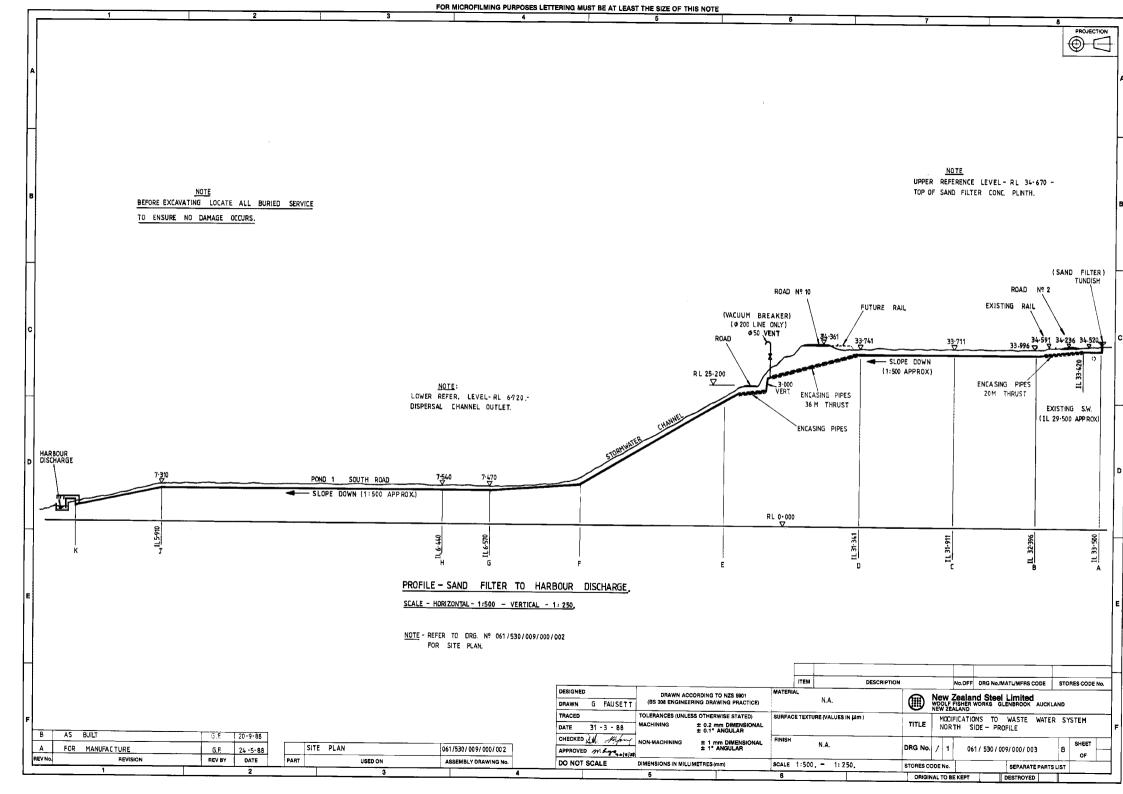


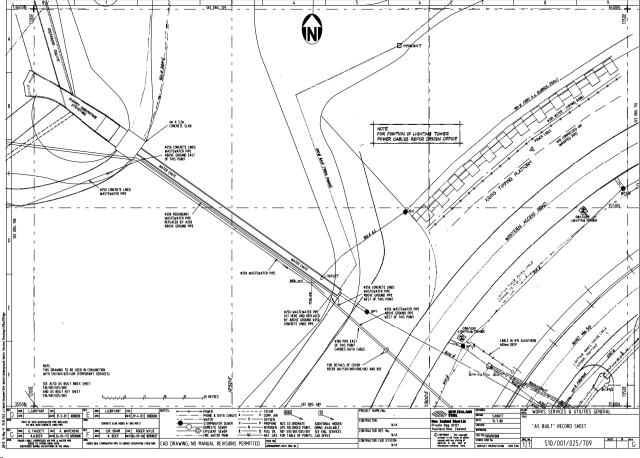
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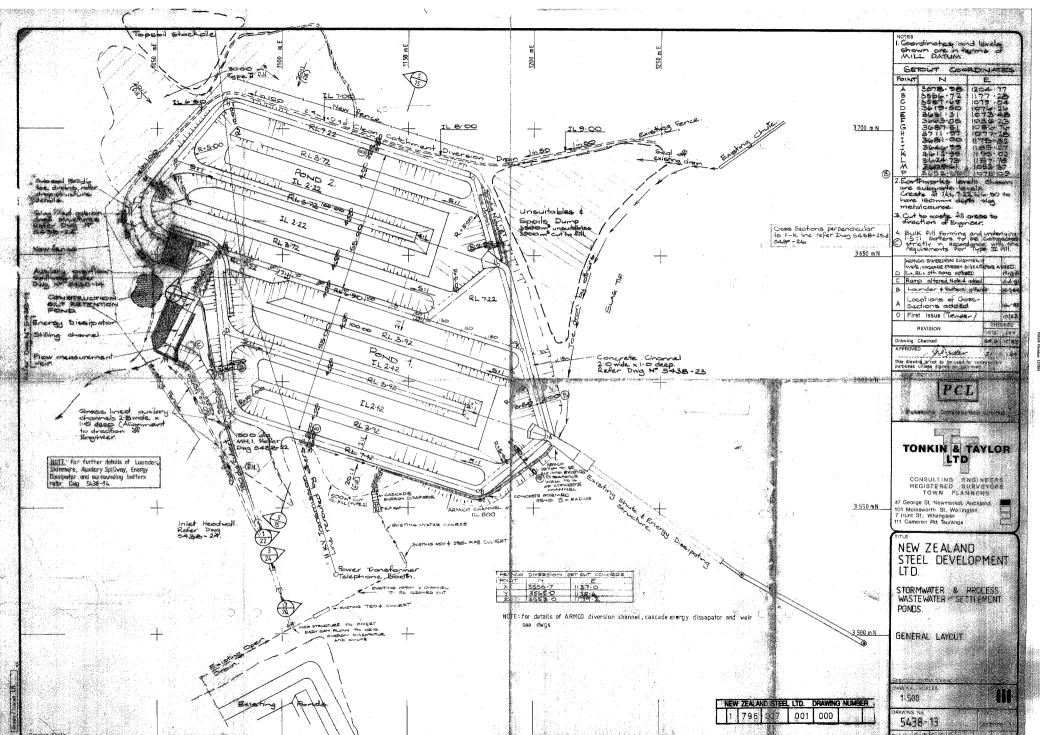
# Appendix C: Drawings





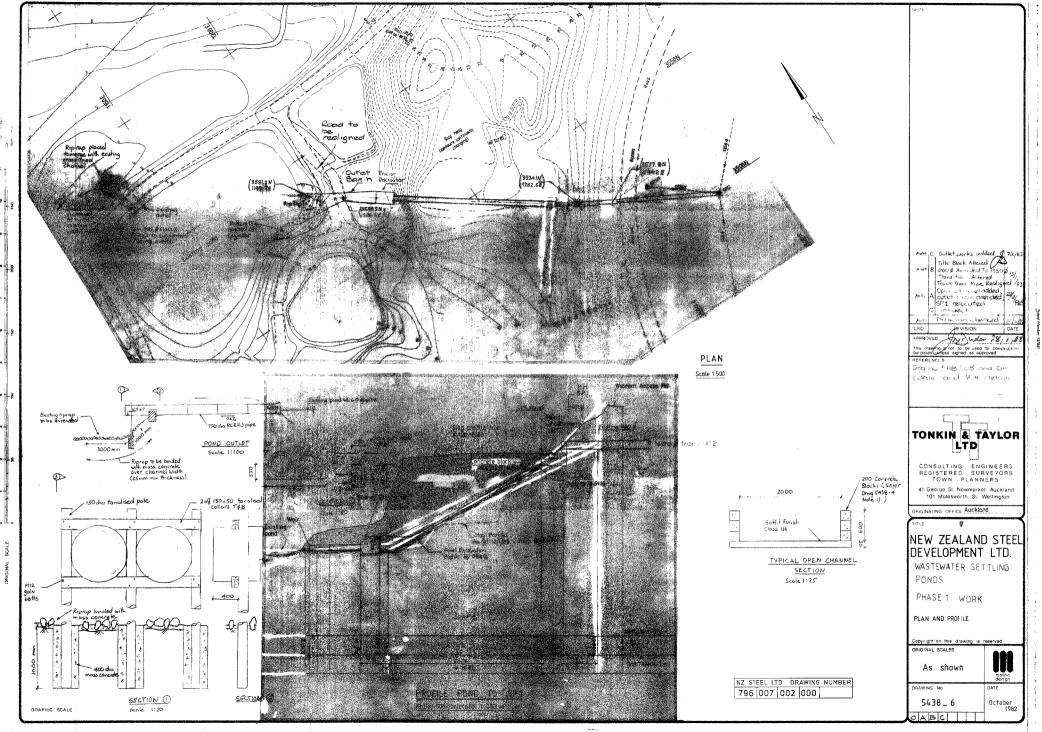




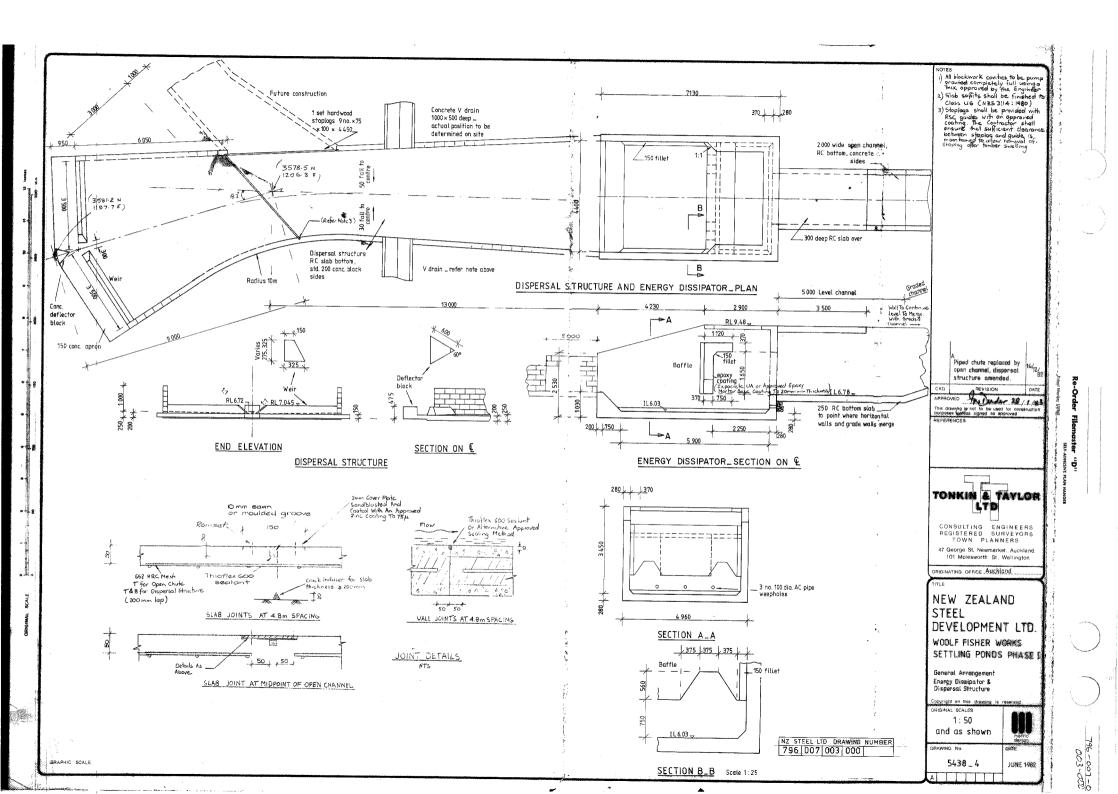


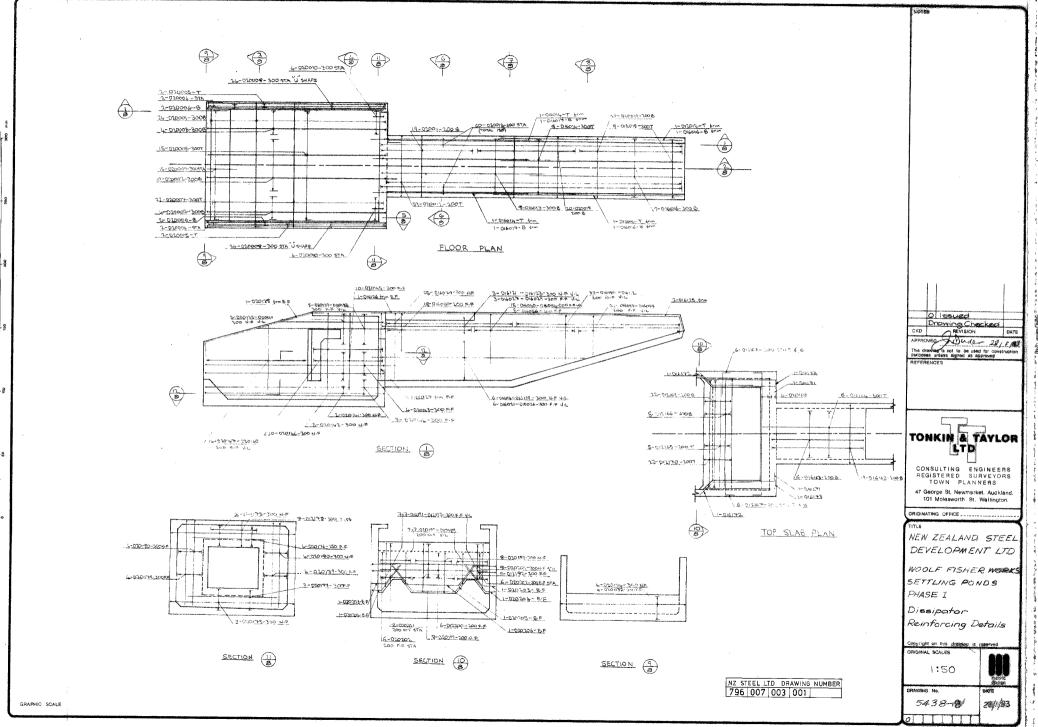
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